

Considerations on Ranging in NGV

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Abstract

Considerations on Ranging in NGV given PAR and use case baseline:

- **Analysis method: Lower Bounds**
- **Observation model: AWGN and line of sight (LOS) free space path loss**
- **5.9 GHz band:**
 - Waveform analysis
 - Time-of-arrival (TOA) vs. round-trip-delay (RTD) ranging
 - Bandwidth and different numerologies
- **60 GHz band:**
 - Comparison between RTD ranging and Radar
 - Dynamic Train-to-Train Propagation Measurements and ranging results

Introduction

PAR [1]:

“this amendment defines procedures for at least one form of positioning in conjunction with V2X communications”

Use Case (UC) baseline document [2]:

- UC5 Vehicular Positioning & Location
- UC8 Train-to-Train
- UC9 Vehicle-to-Train

Lower Bounds Evaluation Methodology: Benefits

[3], [4], [5]:

- **Knowledge and understanding about an estimation problem**
 - Effect of nonlinearities
 - Identification of limiting factors
- **Estimator efficiency**
 - Evaluation of suboptimal estimators
- **System parameter optimization**
 - Allocation of signal power
 - Waveform design
 - Placement of road side units

Lower Bounds Evaluation Methodology: Non-random Parameter Estimation

- Classical definition estimator parameter vector observation vector

$$\underbrace{\mathbb{E}_{\mathbf{y}|\boldsymbol{\theta}} \left[(\hat{\boldsymbol{\theta}}(\mathbf{y}) - \boldsymbol{\theta})(\hat{\boldsymbol{\theta}}(\mathbf{y}) - \boldsymbol{\theta})^T \right]}_{\text{MSE Matrix}} \geq \mathbf{B}_C$$

parameter vector given

- Cramér-Rao Lower Bound (CRLB) for unbiased estimators

$$\text{Cov}(\hat{\boldsymbol{\theta}}) \geq \mathbf{J}_F^{-1}(\boldsymbol{\theta}) \quad [\mathbf{J}_F]_{ij} = -\mathbb{E}_{\mathbf{y}|\boldsymbol{\theta}} \left[\underbrace{\frac{\partial^2}{\partial \theta_i \partial \theta_j} \ln p(\mathbf{y}|\boldsymbol{\theta})}_{\text{log-likelihood of observation vector}} \right]$$

Fisher Information Matrix

- Biased CRLB usually dependent on unknown estimator bias
- Over optimistic for many scenarios

log-likelihood of
observation vector

Lower Bounds Evaluation Methodology: Random Parameter Estimation

- **Bayesian definition** $\text{MSE} = \mathbb{E}_{\mathbf{y}, \boldsymbol{\theta}} \left[(\hat{\boldsymbol{\theta}}(\mathbf{y}) - \boldsymbol{\theta})(\hat{\boldsymbol{\theta}}(\mathbf{y}) - \boldsymbol{\theta})^T \right]$
random parameter vector

- **Ziv-Zakai Lower Bound (ZZLB) [5]**

$$\text{MSE} \geq \frac{1}{2} \int_0^{+\infty} \left\{ \int_{-\infty}^{+\infty} [p(\theta) + p(\theta + h)] P_{\min}(\theta, \theta + h) d\theta \right\} h dh$$

- **Properties of the Bayesian bounds (ZZLB, ...)**
 - Valid for biased estimators
 - Possible to incorporate prior knowledge of the estimated parameters
 - Applicable also to problems that are singular without prior knowledge

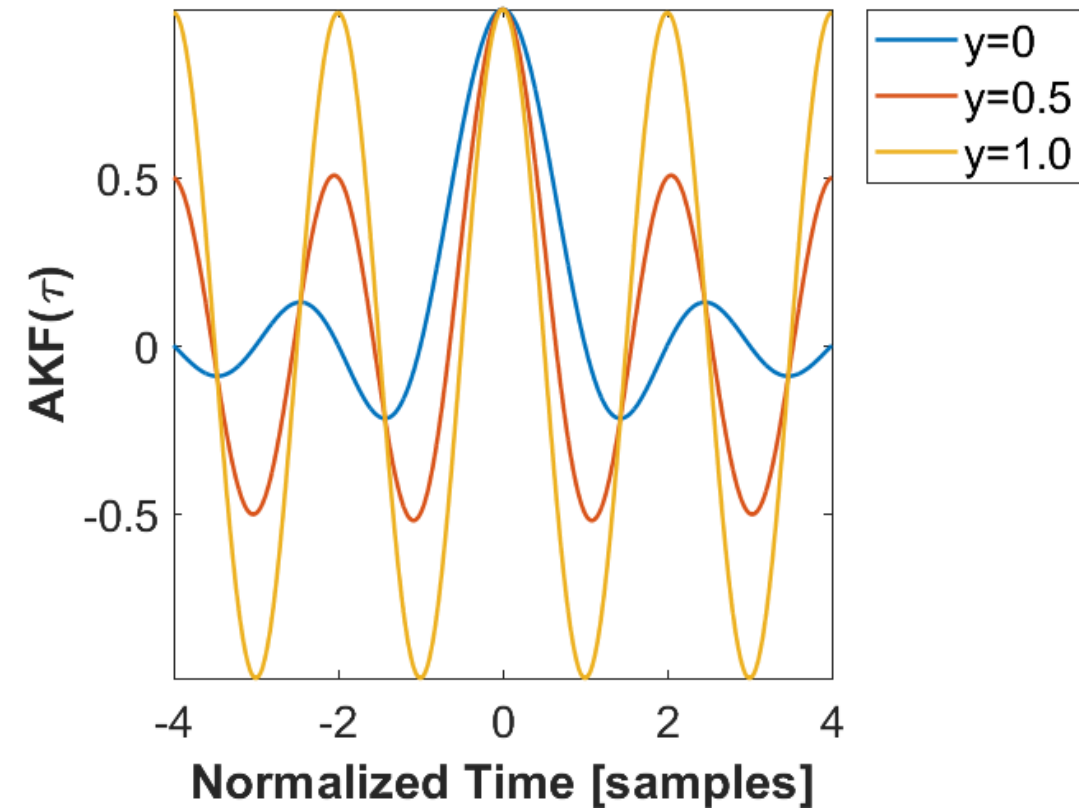
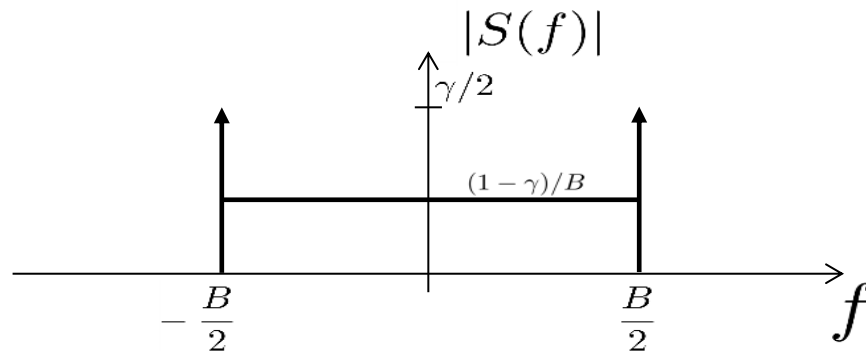
Time-of-Arrival (TOA) Ranging Measurement and Signal Model [6]

- **Observation model: AWGN**

$$y(t) = s(t - \tau) + n$$

- **Signal model (Dirac-Rectangular)**

$$|S(f)|^2 = \begin{cases} \frac{1-\gamma}{B} + \frac{\gamma}{2} \left[\delta\left(f + \frac{B}{2}\right) + \delta\left(f - \frac{B}{2}\right) \right], & |f| \leq \frac{B}{2} \\ 0, & \text{otherwise} \end{cases}$$



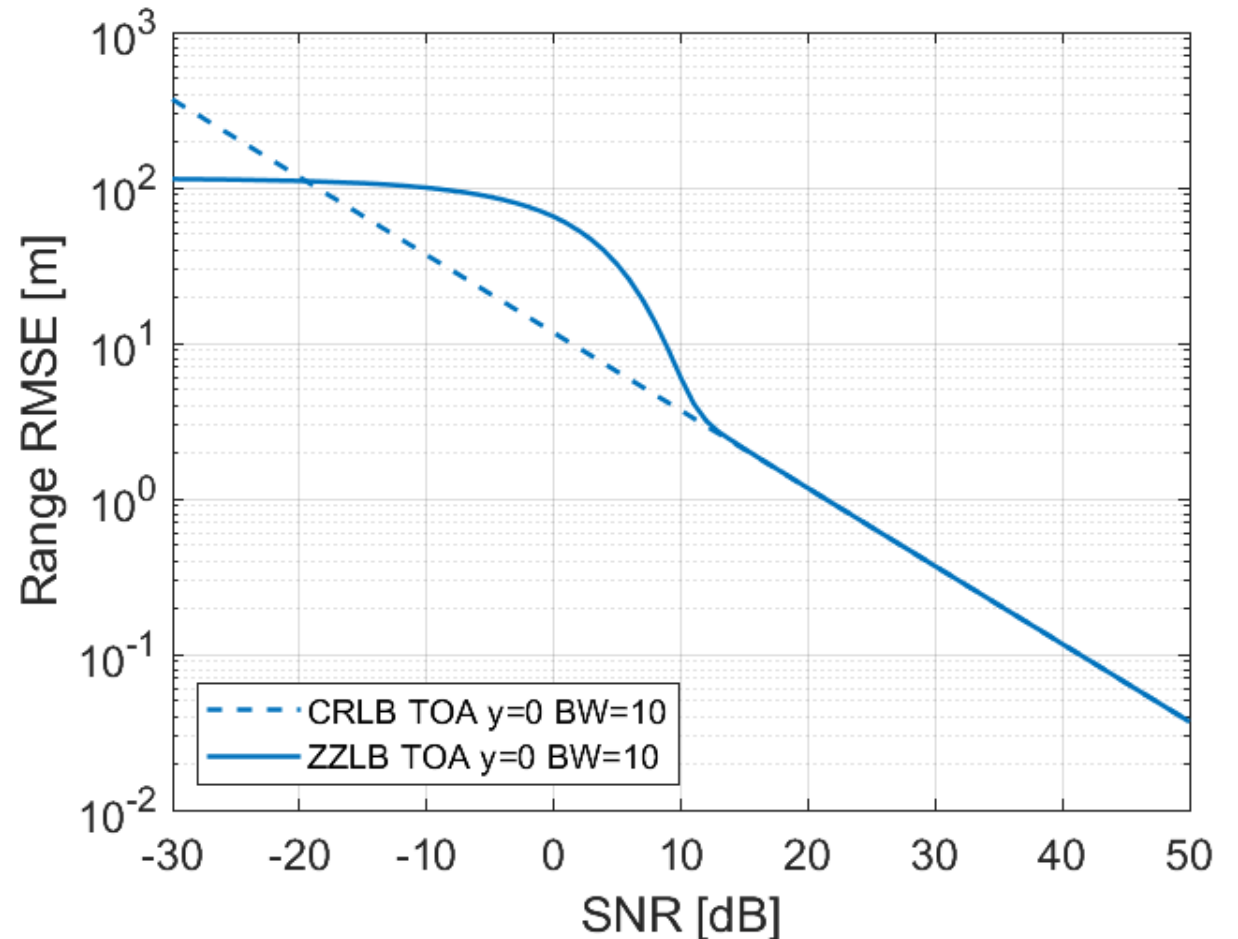
Time-of-Arrival (TOA) Ranging

Lower Bounds [6]

Cramér-Rao Lower Bound (CRLB)
vs . Ziv-Zakai Lower Bound
(ZZLB):

- Same for high SNR
- Rapid increase of ZZLB for medium SNR: Signal ambiguities in observation interval
- Convergence of ZZB to mean of observation interval for low SNR

Note, rectangular waveform ($\gamma=0$)

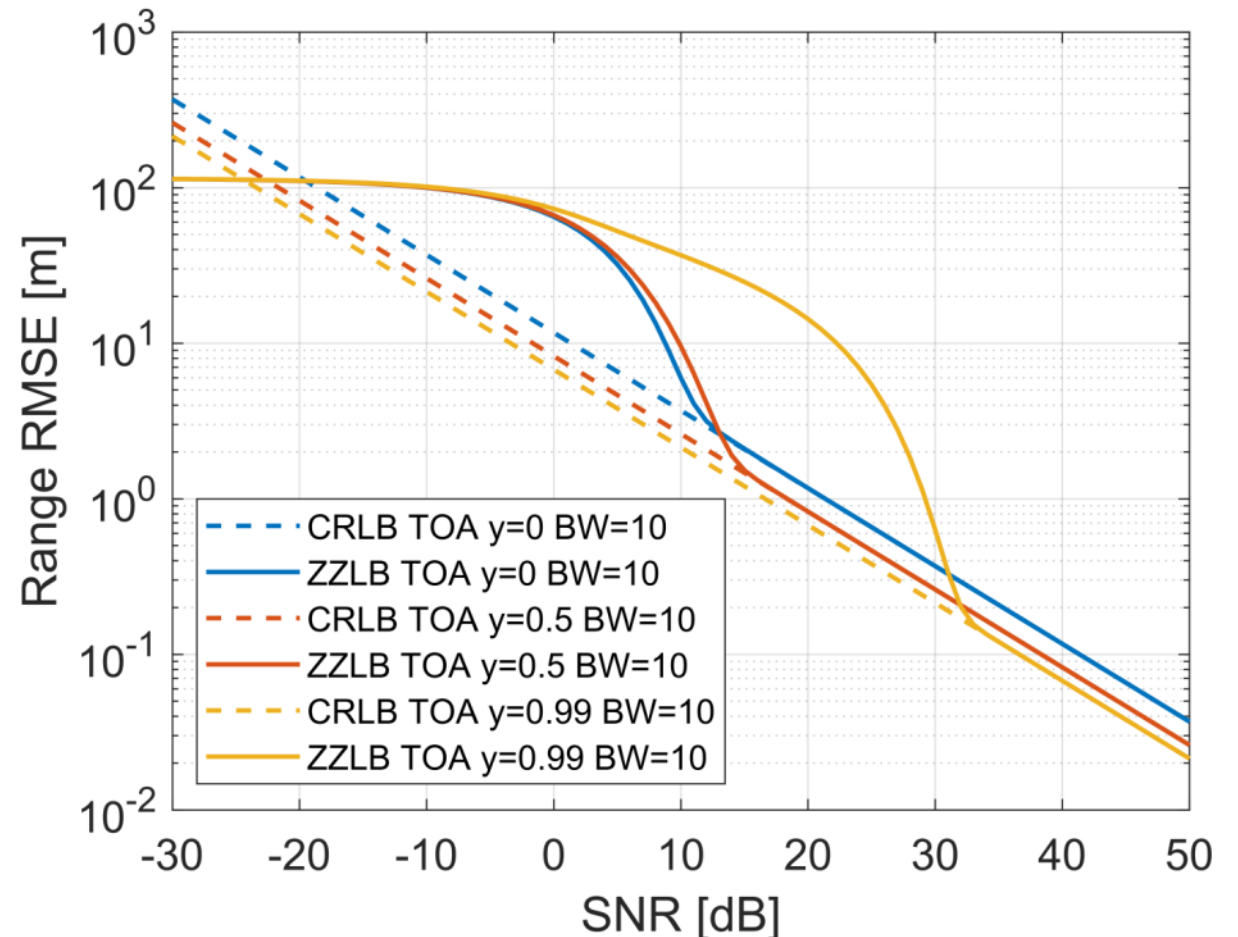
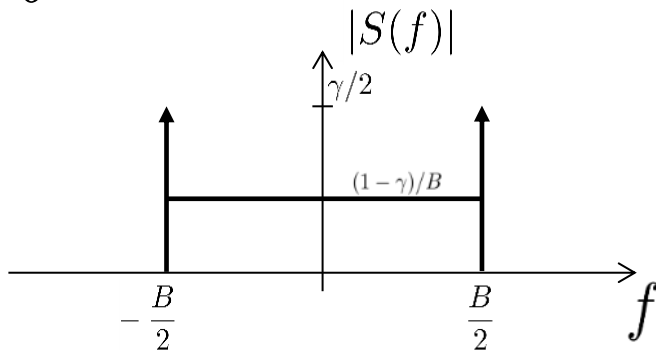


Time-of-Arrival (TOA) Ranging

Lower Bounds [6]

Waveform parameter γ :

- $\gamma=0$, rectangular highest CRLB, ZZLB converges at lowest SNR
- $\gamma=0.5$, 3 dB gain at high SNR, but 2 dB earlier divergence
- $\gamma=0.99$, only 0.2 dB additional gain at high SNR, but divergence 20 dB before $\gamma=0$



Time-of-Arrival (TOA) Ranging Pathloss Model

Line-of-sight (LOS) free space

$$\text{SNR}(d) = \left(\frac{\lambda}{4\pi d} \right)^2 \frac{P_{\text{TX}} G_{\text{TX}} G_{\text{RX}}}{N_{\text{F}} k_{\text{B}} T_{\text{N}} B_{\text{W}}}$$

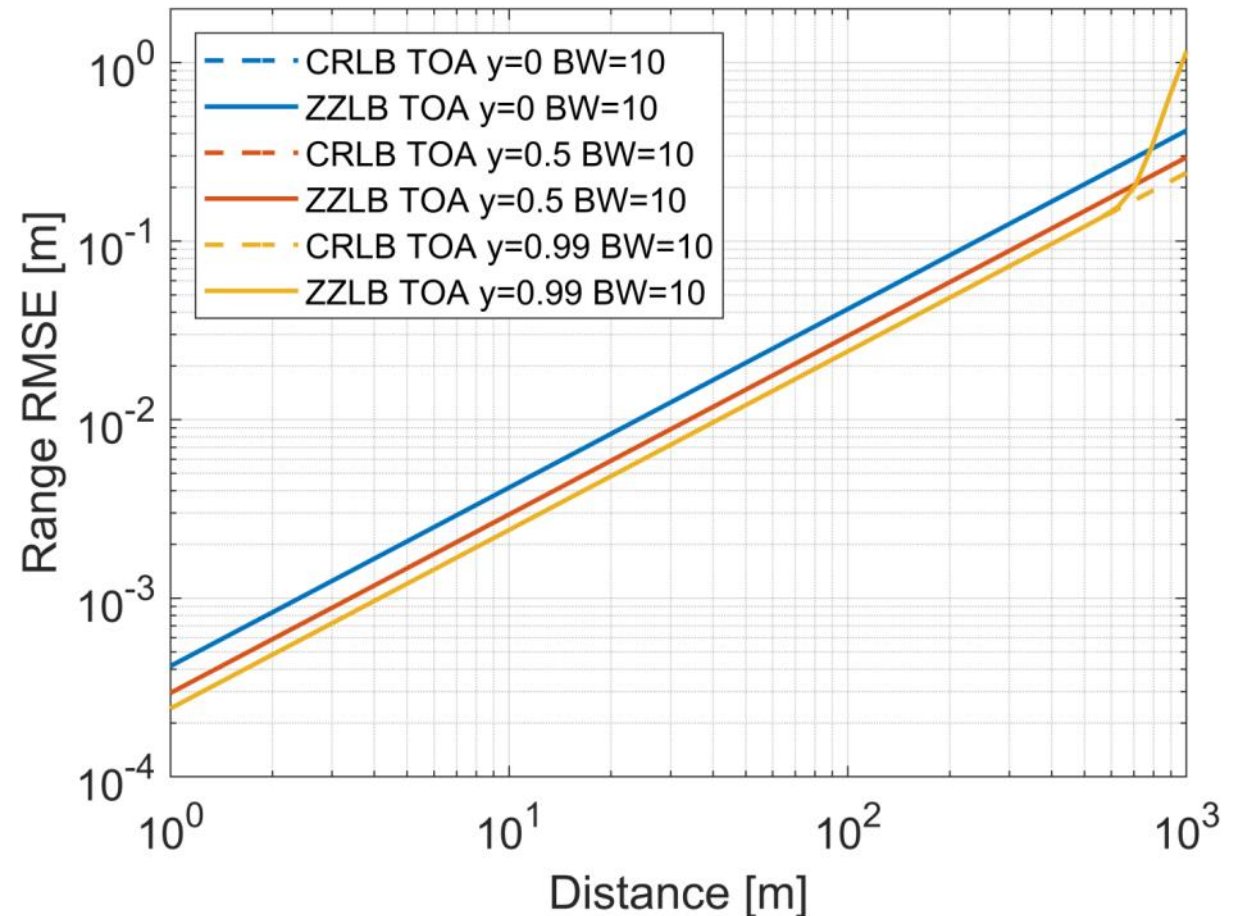
$f_{\text{c}} = 5.9 \text{ GHz}$, $B_{\text{W}} = 10 \text{ MHz}$,

$P_{\text{TX}} G_{\text{TX}} = 33 \text{ dBm}$,

$G_{\text{RX}} = 5\text{dBi}$, $N_{\text{F}} = 5\text{dB}$,

$T_{\text{N}} = 300\text{K}$,

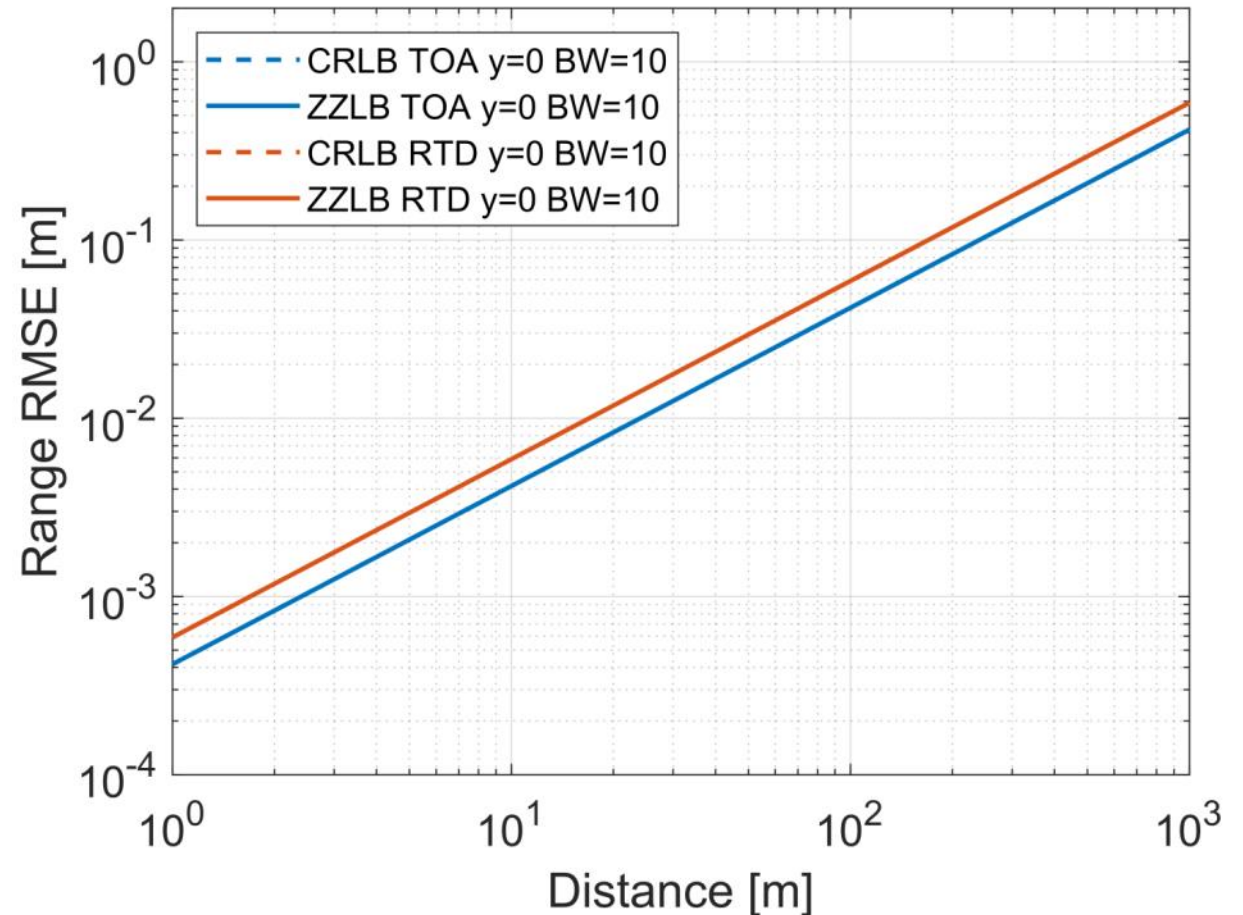
k_{B} Boltzmann constant



Time-of-Arrival (TOA) vs. Round-Trip-Delay (RTD) Ranging

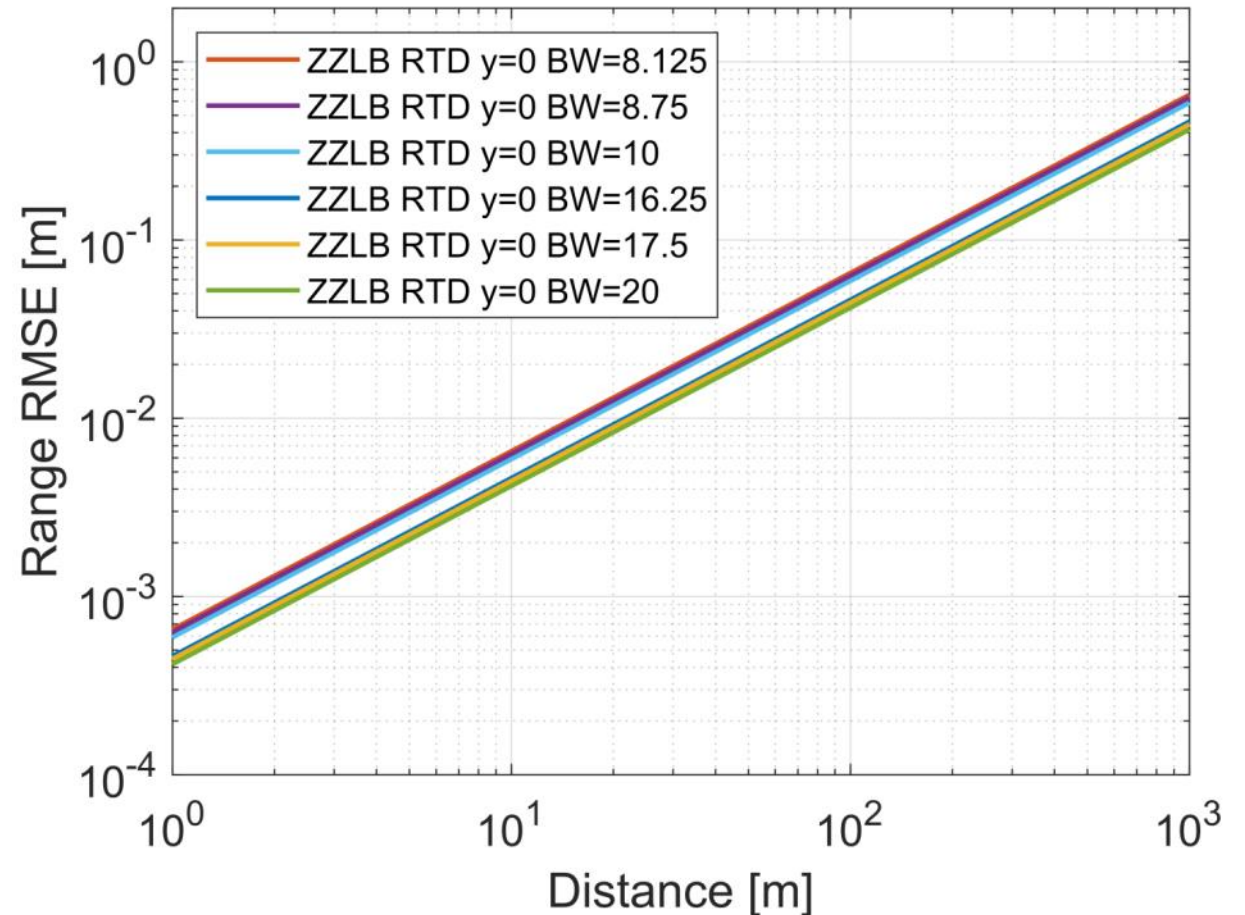
- TOA: Synchronized transmitter and receiver
- RTD: No synchronization required, stable oscillators and clocks for duration of message exchange
- RTD model: Two independent TOA measurements

Note, rectangular waveform ($\gamma=0$) for remaining slides



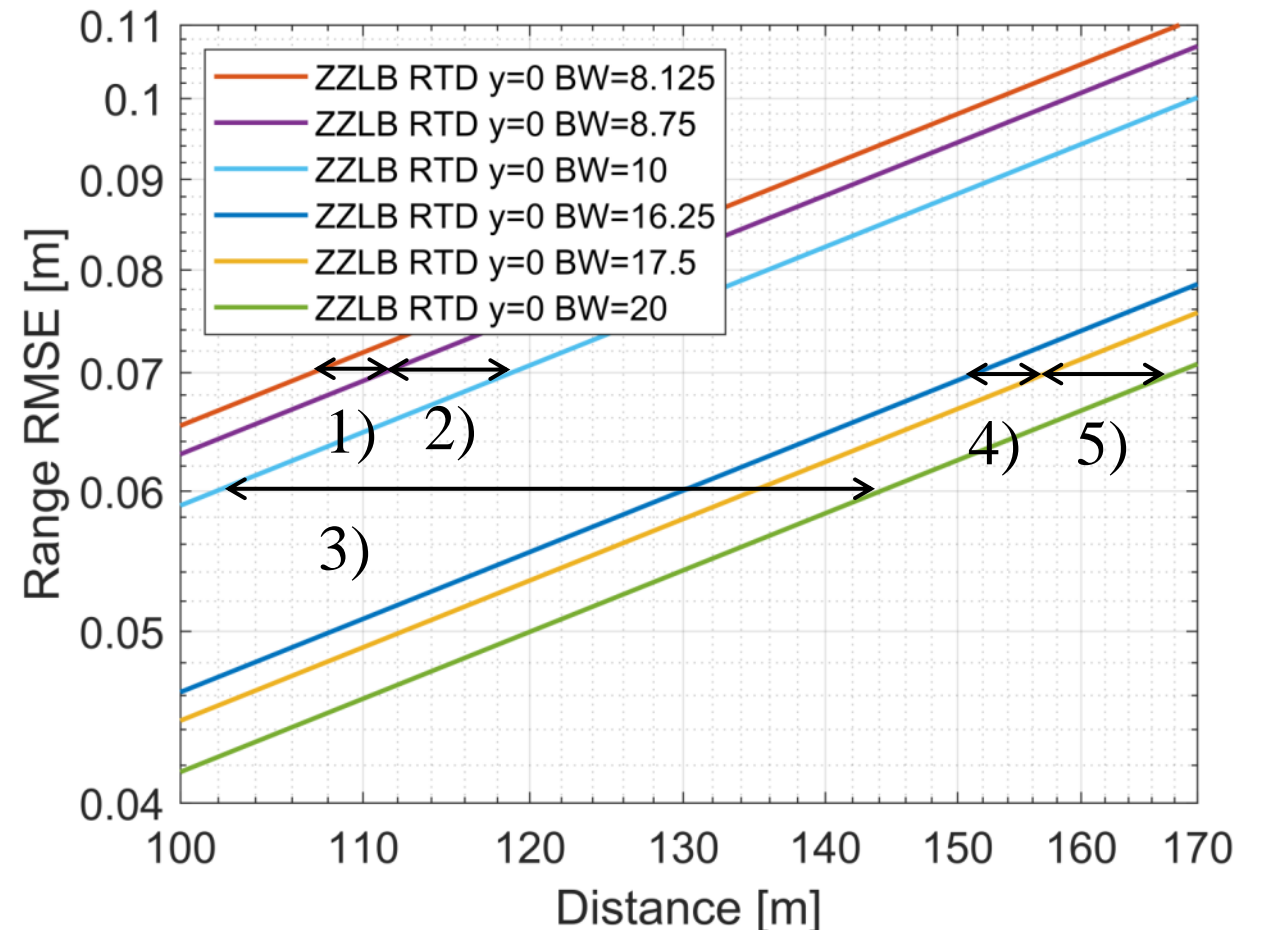
Round-Trip-Delay (RTD) Ranging Bandwidth

- 8.125 MHz = 52 subcarriers
- 8.75 MHz = 56 subcarriers
- 10 MHz = 64 subcarriers
- 16.25 MHz = 52 subcarriers
- 17.5 MHz = 56 subcarriers
- 20 MHz = 64 subcarriers



Round-Trip-Delay (RTD) Ranging Bandwidth

- 1) 4% accuracy gain for
52 → 56 subcarriers 10 MHz
- 2) 7% accuracy gain for
56 → 64 subcarriers 10 MHz
- 3) 30% accuracy gain
10 MHz → 20 MHz
- 4) 4% accuracy gain for
52 → 56 subcarriers 20 MHz
- 5) 7% accuracy gain
56 → 64 subcarriers 20 MHz



Millimeter Wave Round-Trip-Delay (RTD) Ranging and Radar

- Communication, RTD ranging

$$\text{SNR}(d) = \left(\frac{\lambda}{4\pi d} \right)^2 \frac{P_{\text{TX}} G_{\text{TX}} G_{\text{RX}} N_{\text{Avg}}}{L_{d_0} (d/d_0) N_{\text{F}} k_{\text{B}} T_{\text{N}} B_{\text{W}}}$$

$$f_{\text{c}} = 63.5, 76.5 \text{ GHz}, P_{\text{TX}} G_{\text{TX}} = 40 \text{ dBm},$$

$$L_{d_0} = 17.5, 0.2 \text{ dB}, B_{\text{W}} = 1 \text{ GHz}, N_{\text{Avg}} = 1000,$$

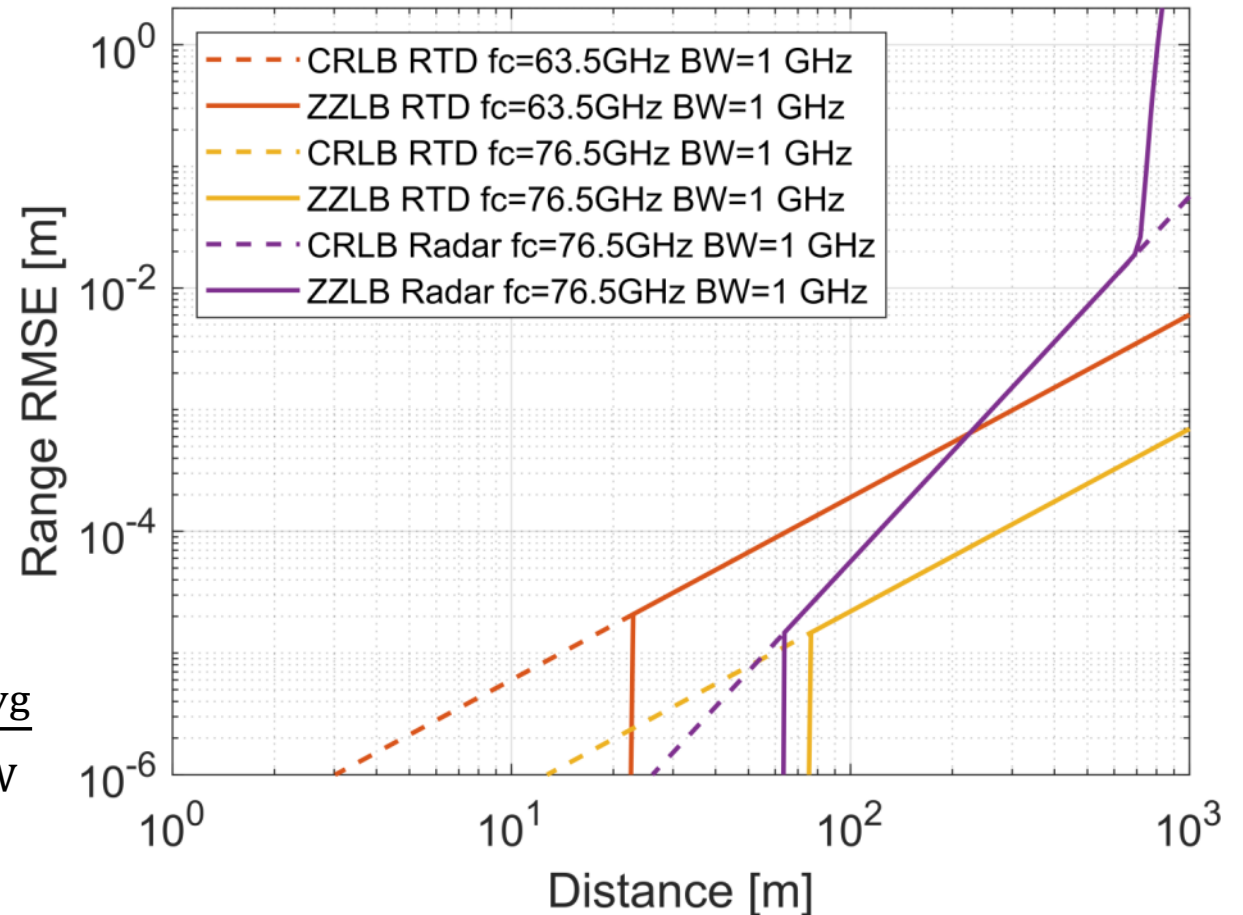
$$d_0 = 2 \text{ km}, G_{\text{RX}} = 23 \text{ dBi}, N_{\text{F}} = 5 \text{ dB}, T_{\text{N}} = 300 \text{ K},$$

- Radar [7]

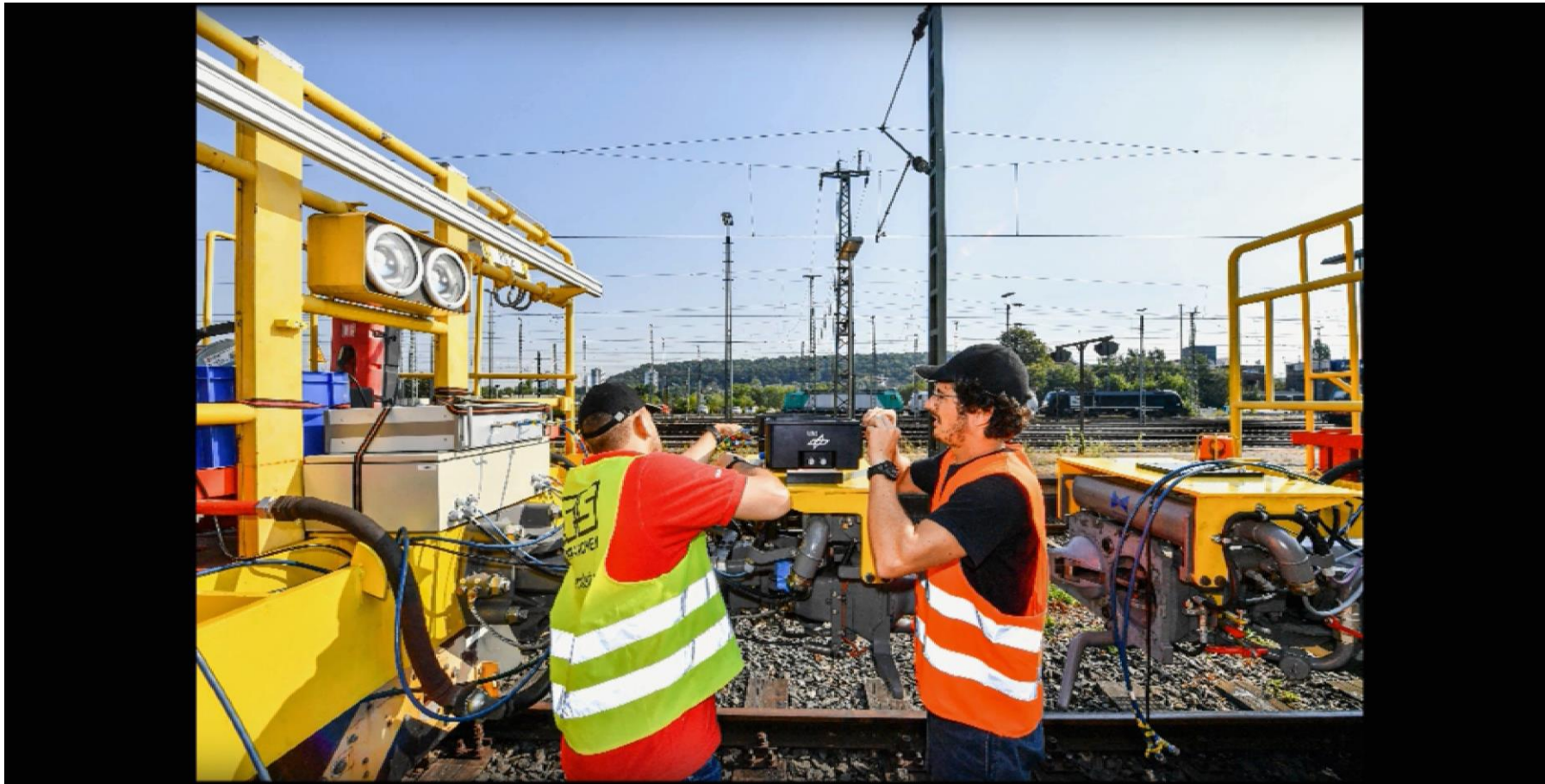
$$\text{SNR}(d) = \left(\frac{\lambda}{L_{d_0} d^3 / d_0} \right)^2 \frac{P_{\text{TX}} G_{\text{TX}} \sigma_{\text{c}} G_{\text{RX}} N_{\text{Avg}}}{(4\pi)^3 N_{\text{F}} k_{\text{B}} T_{\text{N}} B_{\text{W}}}$$

$$f_{\text{c}} = 76.5 \text{ GHz}, L_{d_0} = 0.2 \text{ dB}, \sigma_{\text{c}} = 100 \text{ m}^2,$$

$$P_{\text{TX}} G_{\text{TX}} = 50 \text{ dBm}, k_{\text{B}} \text{ Boltzmann constant}$$

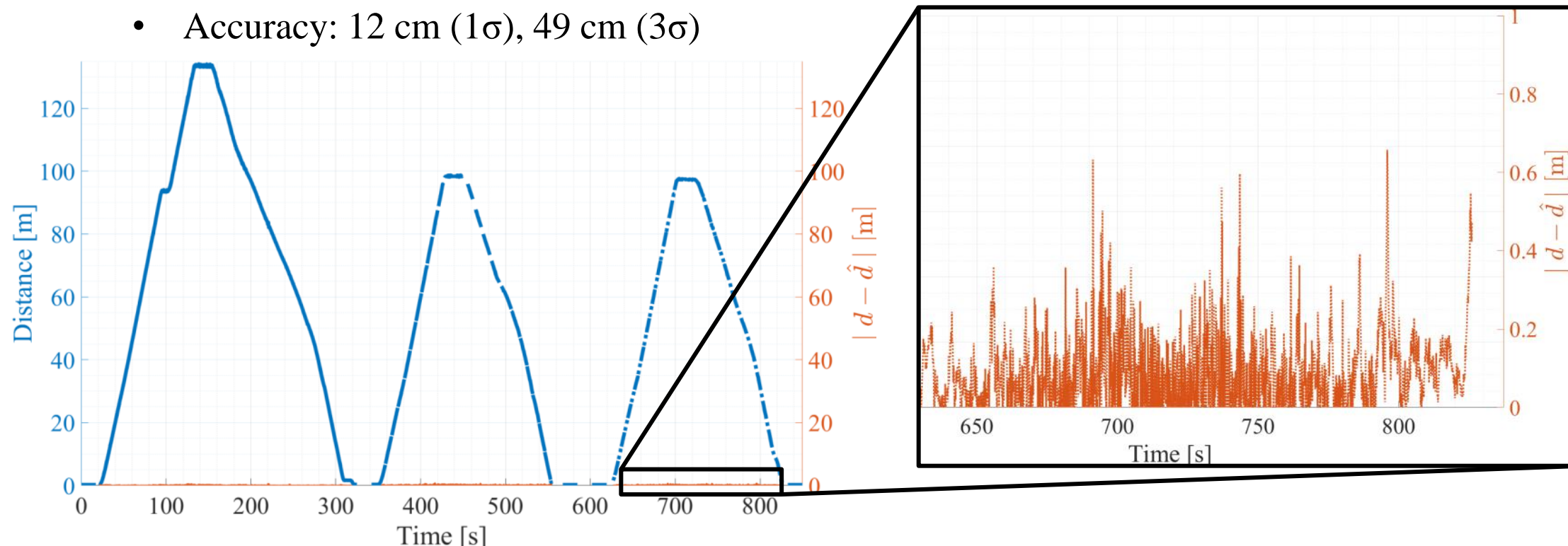


Dynamic Train-to-Train Propagation Measurements in the Millimeter Wave Band [8]



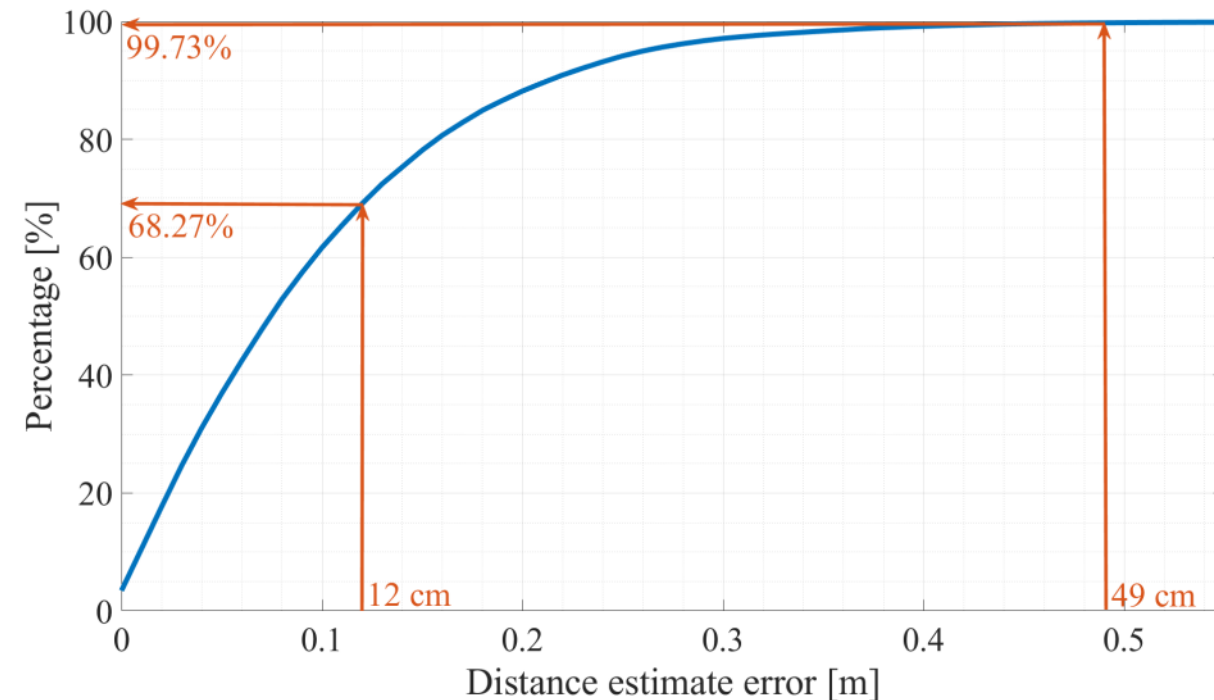
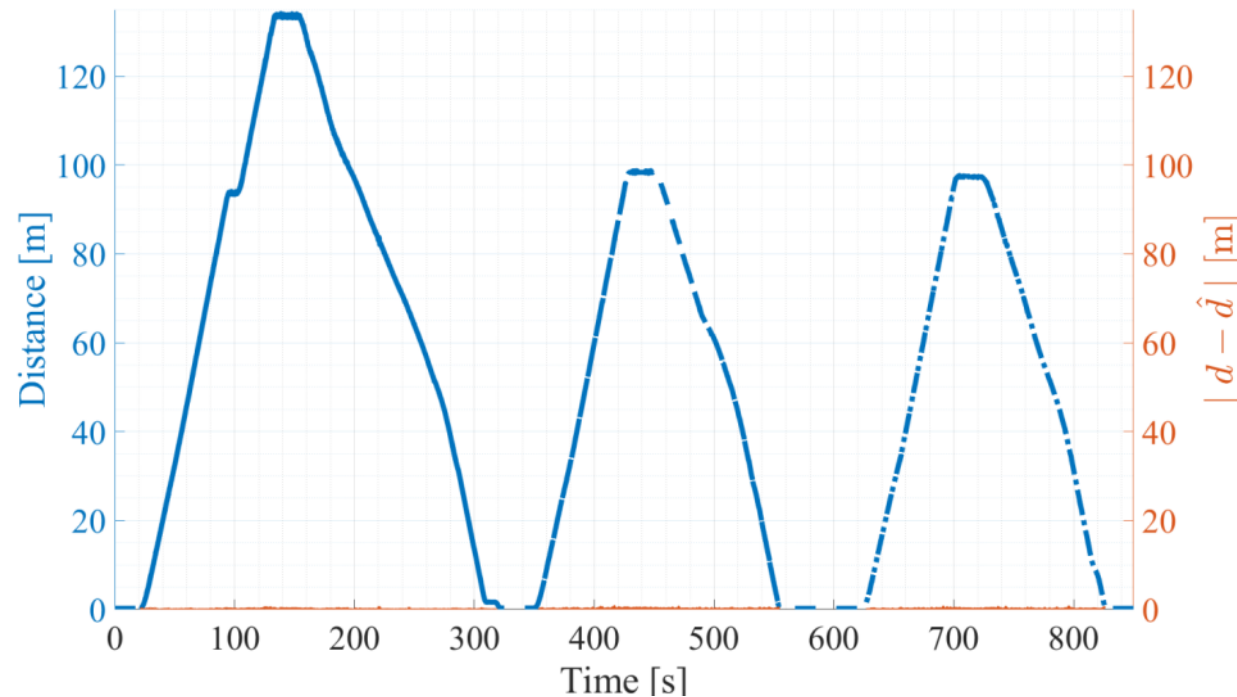
Dynamic Train-to-Train Propagation Measurements in the Millimeter Wave Band [8]

- $f_c = 60$ GHz, $B_W = 120$ MHz
- Snapshot based distance estimator
- Accuracy: 12 cm (1σ), 49 cm (3σ)



Dynamic Train-to-Train Propagation Measurements in the Millimeter Wave Band [8]

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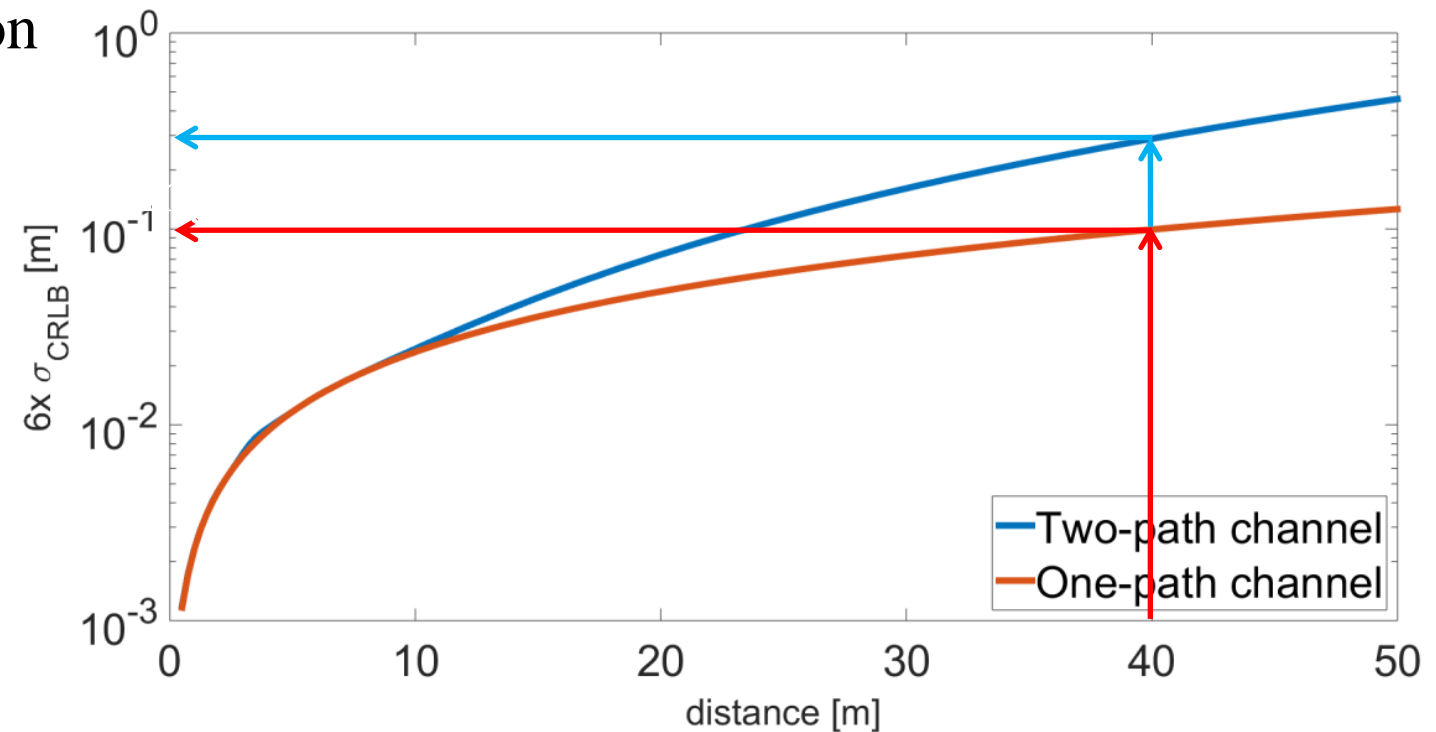
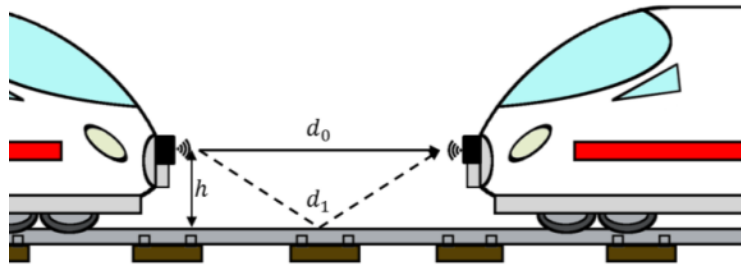
Conclusions

- Bounds
 - Cramér-Rao Lower Bound (CRLB) vs. Ziv-Zakai Lower Bound (ZZLB):
 - CRLB simple, analytic solution vs. ZZLB more complex, numerical solution
 - CRLB and ZZLB same for high SNR
 - CRLB optimistic for low to medium SNR vs. ZZLB tighter at medium to low SNR (accounts for ambiguities)
 - Observation model: Simple model → analytic solution for bounds, but overly optimistic
 - Waveform: Put energy towards band edge, e.g. 50% → 3 dB gain
 - Free Space LoS Pathloss Model @ 5.9 GHz → submeter accuracy
 - RTD 3dB performance loss compared to TOA, no synchronization required
 - Bandwidth comparison: marginal gain for different numerologies, significant gain for 20 MHz vs. 10 MHz
 - Millimeter Wave 63.5 GHz RTD ranging outperforms Radar 76.5 GHz @ distances > 230 m
- Millimeter Wave moving train measurements: 120 MHz BW → 12 cm ranging error @ 1 sigma

Outlook

More realistic observation models

- Multipath, e.g. ground reflection



- Clock and oscillator errors

References

- [1] TGbd, “Project Authorization Request (PAR)”, IEEE 802.11-18/0861r9
- [2] NGV SG, “Use Case Baseline Document Approved By SG”, IEEE 802.11-18/1323r2
- [3] S. M. Kay, *Fundamentals of statistical signal processing*. New Jersey: Prentice Hall PTR, 1993.
- [4] H. L. Van Trees, *Detection, estimation, and modulation theory*. John Wiley & Sons, 2004.
- [5] H. L. Van Trees, *Bayesian bounds for parameter estimation and nonlinear filtering/tracking*. John Wiley & Sons, 2007.
- [6] Dammann, Armin and Jost, Thomas and Raulefs, Ronald and Walter, Michael and Zhang, Siwei (2016) *Optimizing Waveforms for Positioning in 5G*. In: IEEE Workshop on Signal Processing Advances in Wireless Communications, SPAWC. IEEE International workshop on Signal Processing advances in Wireless Communications, 3.-6. Jul. 2016, Edinburgh, UK. DOI: 10.1109/SPAWC.2016.7536783
- [7] Schmidhammer, Martin and Gentner, Christian and Siebler, Benjamin (2019) *Localization of Discrete Mobile Scatterers in Vehicular Environments Using Delay Estimates*. 2019 International Conference on Location and GNSS (ICL-GNSS), 4.-6. Juni 2019, Nuremberg, Germany.
- [8] Soliman, Mohammad and Unterhuber, Paul and Sand, Stephan and Staudinger, Emanuel and Shamsboom, Jeries and Schindler, Christian and Dekorsy, Armin (2019) *Dynamic Train-to-Train Propagation Measurements in the Millimeter Wave Band - Campaign and First Results*. EuCAP 2019, 31 March - 5 April 2019, Krakow, Poland.

Straw Poll #1

Do you agree to add that 802.11bd in the 5.9 GHz band supports round-trip-delay (RTD) ranging for 10 MHz and 20 MHz bandwidth PPDU's?

Yes/No/Abstain: 17/0/2

Straw Poll #2

Do you agree to add that 802.11bd in the 60 GHz band supports round-trip-time (RTT) ranging for TBD Hz bandwidth PPDU's?

Yes/No/Abstain: